



## Paper-based pump-free magnetophoresis†

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Microfluidic magnetophoresis is a powerful technique that is used to separate and/or isolate cells of interest from complex matrices for analysis. However, mechanical pumps are required to drive flow, limiting portability and making translation to point-of-care (POC) settings difficult. Microfluidic paper-based analytical devices ( $\mu$ PADs) offer an alternative to traditional microfluidic devices that do not require external pumps to generate flow. However,  $\mu$ PADs are not typically used for particle analysis because most particles become trapped in the porous fiber network. Here we report the ability of newly developed fast-flow microfluidic paper-based analytical devices (ffPADs) to perform magnetophoresis. ffPADs use capillary action in a gap between stacked layers of paper and transparency sheets to drive flow at higher velocities than traditional  $\mu$ PADs. The multi-layer ffPADs allow particles and cells to move through the gap without being trapped in the paper layers. We first demonstrate that ffPADs enable magnetic particle separations in a  $\mu$ PAD with a neodymium permanent magnet and study key factors that affect performance. To demonstrate utility, *E. coli* was used as a model analyte and was isolated from human urine before detection with a fluorescently labeled antibody. A capture efficiency of 61.5% was then obtained of *E. coli* labeled magnetic beads in human urine. Future studies will look at the improvement of the capture efficiency and to make this assay completely off-chip without the need of a fluorescent label. The assay and device described here demonstrate the first example of magnetophoresis in a paper based, pump free microfluidic device.

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## 1. Introduction

Improving medical diagnostics is a key need to reduce the 15 million deaths a year from infectious diseases.<sup>1</sup> While significant improvement has been made in the field, patients in many parts of the world still cannot access early diagnosis which is crucial for adequate care.<sup>2–5</sup> For example, sepsis patients treated within one day of showing symptoms had a 10% mortality rate, while those treated after three days had a 50% mortality rate.<sup>6</sup> Current infectious disease detection methods include culturing, polymerase chain reaction (PCR), and enzyme-linked immunosorbent assay (ELISA).<sup>1,7</sup> These methods are widely accepted because of their ability to detect bacteria with low limits of detection.<sup>8–10</sup> However, all require trained personnel, can take days to weeks to complete, and cost at least \$10 per test.<sup>11</sup> Consequently, a simple, rapid, and

reliable point-of-care (POC) diagnostic for the detection of infectious diseases that is both sensitive and selective is needed. Land *et al.* recently recommended POC technologies to meet a REAS-SURED criteria.<sup>12</sup> These criteria are defined as real-time connectivity, ease of specimen collection, affordable, sensitive, specific, user-friendly, rapid and robust, and equipment-free.  $\mu$ PADs are one technology that meets many of these requirements but suffers from slow fluid velocity and poor limits of detection.<sup>2,13</sup> One technique known to improve detection limits and selectivity of an assay is to separate target analytes from the sample matrix.<sup>14</sup>

In this work, we are focused on isolating bacteria from complex matrices to remove interferences, concentrate the target cells, and improve detection performance. The cell separation/isolation process can be tedious, so microfluidic platforms have been developed to automate and simplify this process.<sup>15</sup> A popular microfluidic separation approach is magnetophoresis, which separates cells in continuous flow using a permanent magnet to move magnetically labeled cells from one flowing stream to another.<sup>16</sup> However, magnetophoresis requires external pumps to drive flow, limiting their portability and usefulness for POC applications.  $\mu$ PADs transport fluid *via* capillary action, which eliminates the need for external pumps,<sup>17</sup> but are not currently used for magnetophoresis because particles and cells become trapped in the paper fibers and fluid velocities generated in  $\mu$ PADs are not fast enough for continuous separation.<sup>18</sup> In this work we solve both issues by creating fast flow in a modified multi-layer

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$\mu$ PAD.<sup>2,13,19–21</sup> Fast-flow  $\mu$ PADs (ffPADs) are created by stacking two layers of wax-printed paper around laser cut double sided adhesive to create channels or gaps. The channels between paper layers enable fast flow without trapping particles. The velocities in the multi-layer  $\mu$ PAD increase by 145 $\times$  or more compared to single-layer  $\mu$ PADs. The fast-flow phenomenon seen with this method of fabrication was characterized in depth previously in Channon *et al.*<sup>19,20</sup> Taking advantage of this fast-flow phenomenon provides a way to make paper-based magnetophoresis possible.<sup>19</sup> Herein we describe the first example of a paper-based, pump-free magnetophoretic device and demonstrate its capabilities by detecting bacteria in urine. We envision the  $\mu$ PAD designed here for rapid detection of *E. coli* and other bacteria and viruses would benefit both food safety and human health diagnostics.

## 2. Materials and methods

### 2.1 Materials

Whatman 1 chromatography paper was purchased from GE Healthcare Sciences. Wax patterns were printed using a Xerox ColorQube 8870 and an IsoTemp hot plate (Fisher Scientific) was used to melt the wax. A benchtop digital microscope (Dino-

Lite AF4915) was used for laminar flow colorimetric experiments. Two fluorescent Dino-Lite digital microscopes with excitation wavelengths of 400 nm and 570 nm (Dino-Lite AM4115T-CFVW and Dino-Lite AM4115T-YFGW) were used for fluorescence detection and analysis. All videos were imported into ImageJ for analysis. A cylindrical  $\frac{1}{4}'' \times \frac{1}{4}''$  Neodymium Iron Boron (NdFeB) permanent magnet, grade N52 (K&J Magnetics, INC.) was used to create an external magnetic field. Other magnet types and shapes were investigated, however the cylindrical magnet was chosen because of the smaller size while maintaining strong field lines. All magnetic beads were purchased from Spherotech Inc. (Lake Forest, Illinois). *E. coli* antibodies (bs-2033R/bs-2033R-A555) were purchased from Bioss Antibodies. The buffers used in this work were 0.1 M phosphate-buffered saline (PBS) and 0.1 M PBS with 0.1% Tween-20 (PBST). The two antibodies were diluted in PBS. Human pooled urine was purchased from Lee Biosolutions (Maryland Heights, MO).

### 2.2 Device design and fabrication

The  $\mu$ PADs discussed here were designed in CorelDRAW X4 and then printed onto Whatman grade 1 chromatography paper and

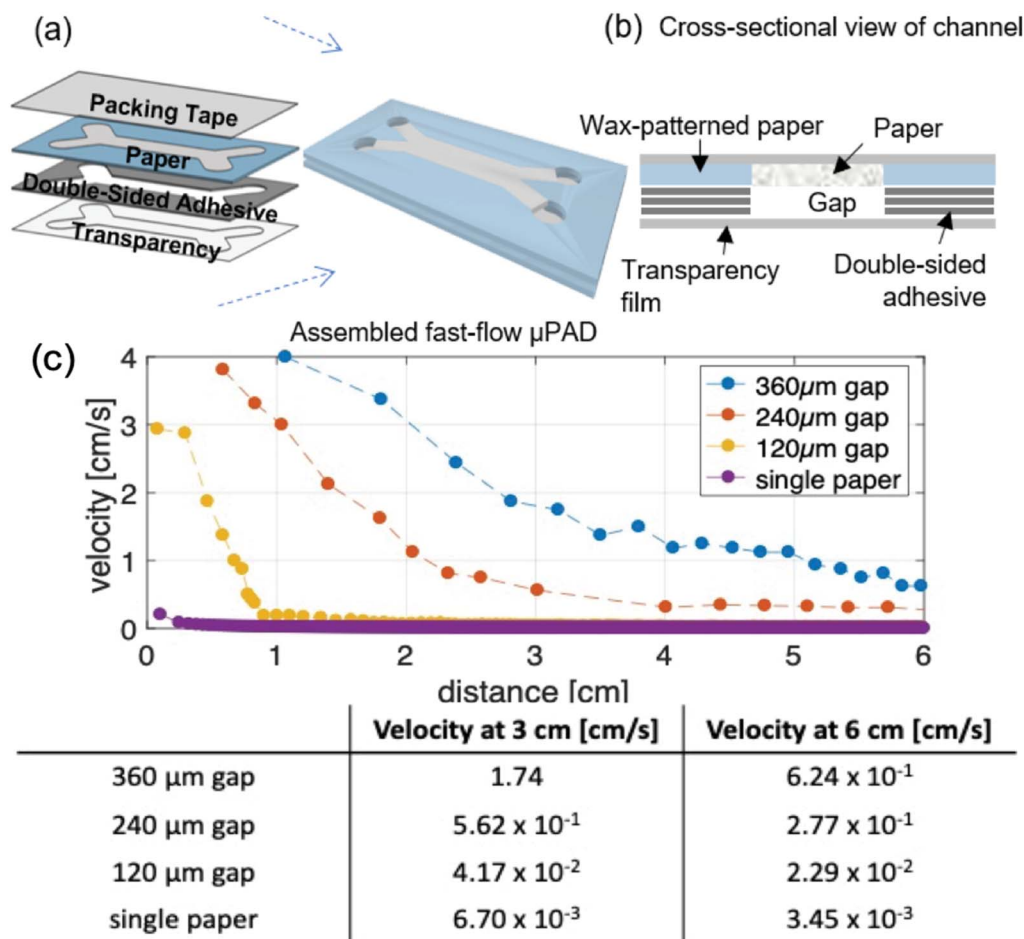


Fig. 1 Assembly and flow characteristics of microfluidic paper-based analytical devices ( $\mu$ PADs) (a) schematic of fast-flow  $\mu$ PAD assembly. (b) Cross-sectional view of channel of fast flow  $\mu$ PADs, with flow to-ward/away from the observer. (c) Plot showing flow velocities with respect to gap height.

a cellulose acetate transparency sheet (3M PP2950). Next the paper was placed on a hot plate at 150 °C for 90 s to create hydrophobic barriers. Grade 467 and 468 double-sided adhesive were used to define the gap height, and the channel pattern was cut out using a CO<sub>2</sub> laser cutter (Epilog Zing Laser Cutter and Engraver). The multilayered device was then assembled in 8.5" × 11" sheets by first applying the double-sided adhesive to the transparency and applying consistent pressure with a pouch laminator set at room temperature. Next, the top paper layer was placed directly onto the double-sided adhesive using a guide to provide necessary alignment to create the ffPAD.

### 2.3 Magnetophoresis system setup

A range of fluorescent carboxyl magnetic particles from 2.0 μm to 44.1 μm were purchased from Spherotech Inc. and diluted from 5 mg mL<sup>-1</sup> to 1 mg mL<sup>-1</sup> in phosphate buffered saline (PBS). All 44.1 μm particles used in these and following studies were labeled with a yellow fluorophore onto the surface of the particles with an excitation wavelength from 400–500 nm and emission from 450–550 nm. Imaging was done with the Dino-Lite microscope (400 nm). All dilutions of particles were made in phosphate-buffered saline, pH 7.2, kept at room temperature and protected from light. Solutions were vortexed for 30 s before use (Scientific Industries Vortex Genie 2). The Grade N52 permanent magnet was placed on top of the device and placement was optimized for consistent and ideal separation results based on magnetic field lines. Images of the fluorescent

particles within the gap of the device were taken using the fluorescent DinoLite microscope.

### 2.4 *E. coli* growth and sample preparation

*E. coli* DH5- $\alpha$  was used as the model bacteria in this work; it was grown in Universal Pre-Enrichment Broth (Sigma-Aldrich, pH 7) overnight in a shaker at 37 °C and 220 rpm. The bacteria concentration was quantified by serial dilution and plating on lysogeny broth (LB) agar plates. Serial dilutions of this solution were made using PBS or human pooled urine.

### 2.5 *E. coli* detection using immunomagnetic separation and H-cell device in human urine

The enzymatic assay presented by Srisa-Art *et al.* was modified for DH5- $\alpha$  detection.<sup>22</sup> The entire assay was performed on the benchtop at room temperature. First, 44.1 μm streptavidin-coated paramagnetic beads (SpheroTech) were vortexed for 30 s at room temperature. Second, the beads were conjugated to a biotinylated anti-*E. coli* antibody in a microcentrifuge for 20 min on a rotator. Third, an immunomagnetic separation (IMS) was performed using a magnet (DynaMag-2 magnet, Thermo Fisher Scientific, Inc.) to isolate and concentrate the magnetic bead-antibody complex by removing the supernatant and resuspending the content in 100 μL of PBS. Fourth, the bead-antibody complex was added to 1 mL of *E. coli* spiked urine and incubated on a rotator for 20 min. Another IMS step was performed to isolate/concentrate the sample and to remove

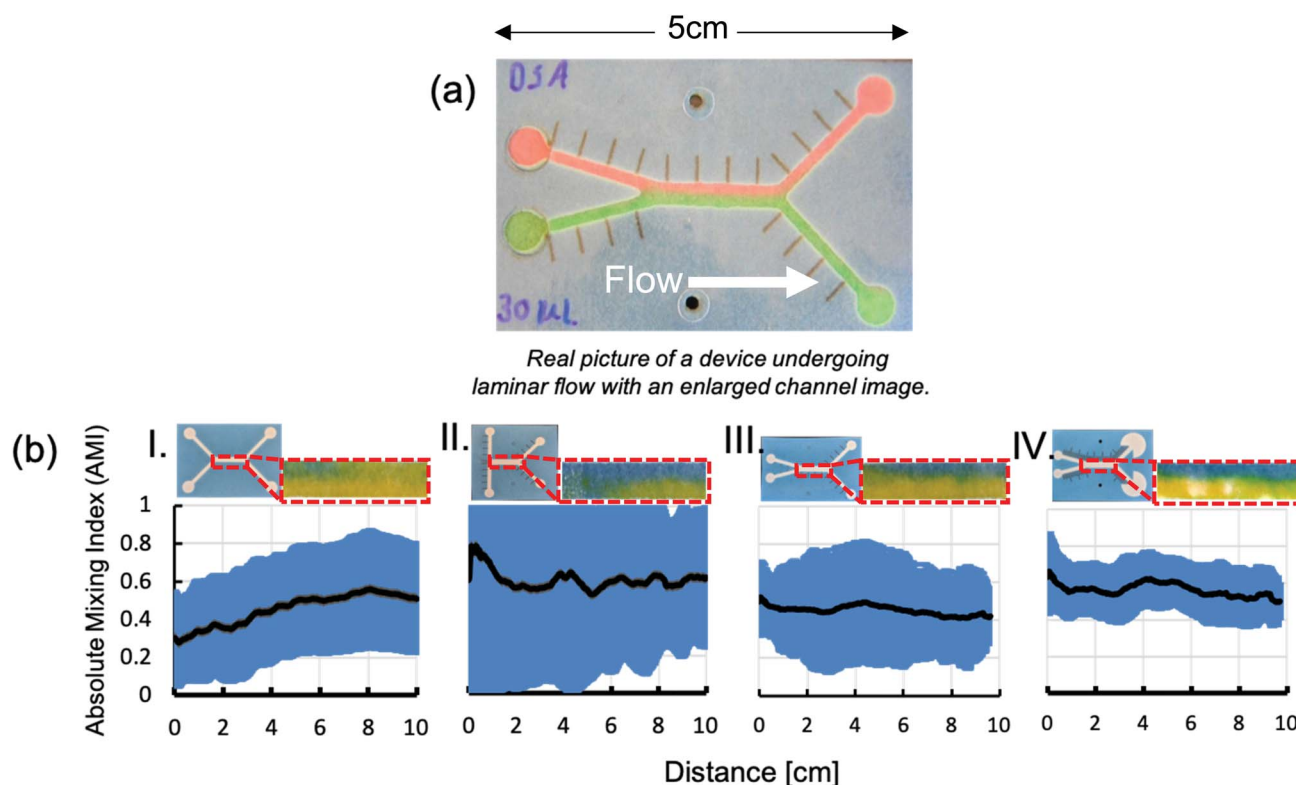


Fig. 2 (a) Image taken of fast-flow  $\mu$ PAD with laminar flow. (b) Images taken of the middle channel to analyze AMI. The corresponding graphs show the effect the angle has on consistency of laminar flow by quantifying the amount of mixing of each device.

the supernatant. The complex was washed twice with PBS-Tween (0.1%) to remove any unbound species. Finally, an anti-*E. coli* Alexa Fluor-555 was conjugated to the bead complex for 20 min on a rotator. The final complex was then washed twice using IMS with PBS-Tween. The complex was then resuspended in 50  $\mu\text{L}$  of urine. 30  $\mu\text{L}$  of the complex was then added simultaneously to the device with 30  $\mu\text{L}$  of PBS buffer to create capillary driven laminar flow. The permanent magnet was placed on the adjacent channel at the desired detection zone. After 30 s the fast-flow has stopped and analysis of *E. coli* capture was performed.

## 2.6 Image analysis

Videos of all experiments were taken with the DinoLite microscopes and pictures were then exported to be analyzed in NIH ImageJ. The images were split into red, green, and blue channels for elimination of background signal and analysis. Fluorescence intensity plots were created with proportional mean grey scale values.

## 3. Results and discussion

### 3.1 Device dimensions and laminar flow

An H-cell device was created from paper and transparency film to demonstrate capillary driven laminar flow was possible. The

device was assembled by stacking packing tape, paper, double-sided adhesive, transparency together as shown in Fig. 1a. Fig. 1b shows the cross-sectional view of the channel once the device is assembled. ffpADs yield faster sustained flows than traditional  $\mu\text{PADs}$ , as demonstrated in Fig. 1c where the liquid 6 cm from the inlet in a ffpAD with 360  $\mu\text{m}$  gap has a speed of  $0.62 \text{ cm s}^{-1}$  versus  $0.0035 \text{ cm s}^{-1}$  in traditional single-layer  $\mu\text{PAD}$ .<sup>19</sup> The gap height can be controlled by changing the number of double-sided adhesive layers placed between the paper and transparency layers. Modeling of this phenomenon recently published by Channon *et al.* describes flow dominated by Laplace pressure for the first 1–2 cm.<sup>20</sup> Shown by a still image in the supplemental, the fluid flow in the gap of the device is dragging the liquid in the paper layer. The flow in the gap is then dominated by a “moving wall” of liquid, resulting in a shear flow within the paper and a linear velocity profile.<sup>19,20</sup> The modeling described is confirmed by the experimental results in Fig. 1c where there are fast initial velocities of over  $4 \text{ cm s}^{-1}$  for a 360  $\mu\text{m}$  gap height that decay over time.<sup>20</sup> The fluid velocities in the devices shown here have similar flow characteristics and show the same experimental results described by Channon *et al.*<sup>19,20</sup> Although ffpADs have shown faster velocities when compared to traditional  $\mu\text{PADs}$ , the maximum Reynolds number (Re) in the multi-layer device was calculated to be 2.0, which occurred in the 360  $\mu\text{m}$  gap

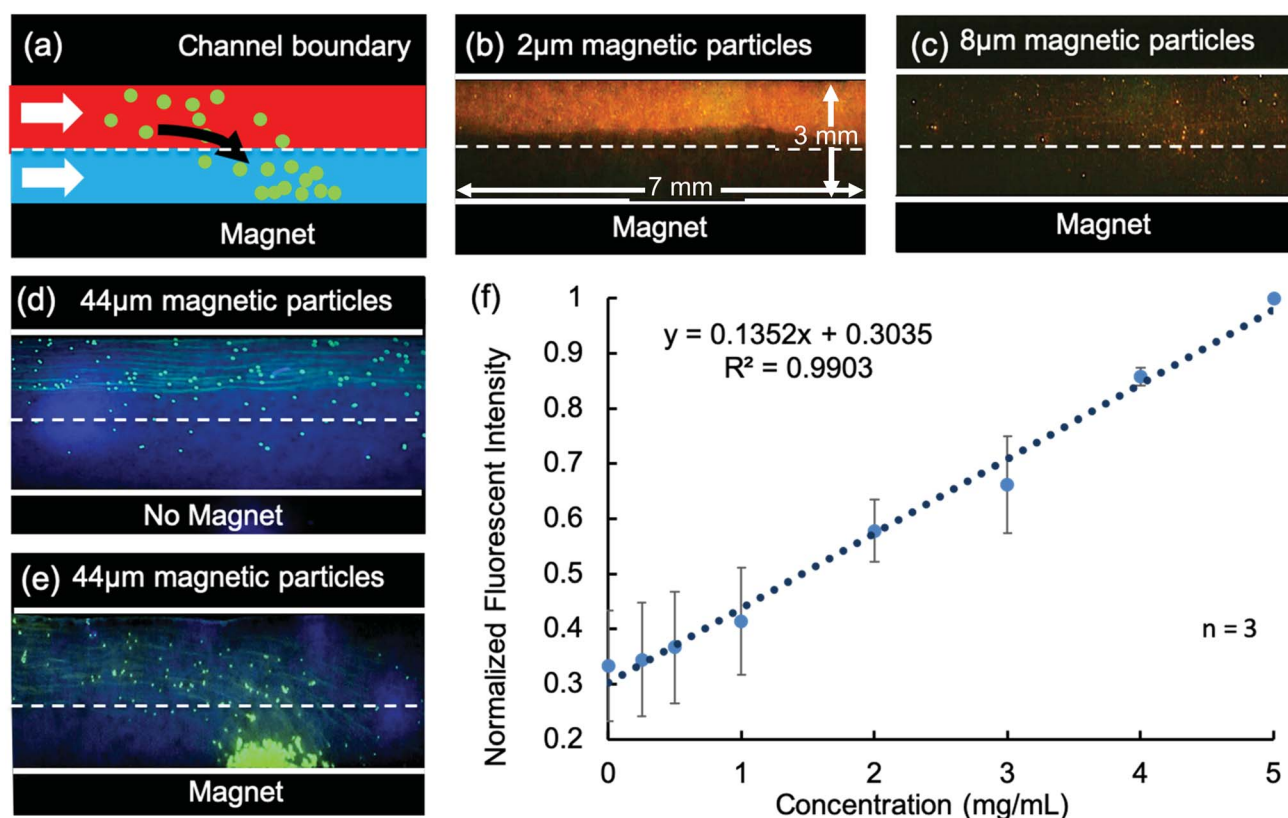


Fig. 3 Magnetophoresis in microfluidic paper-based analytical devices ( $\mu\text{PADs}$ ) (a) overview of magnetophoresis concept, where the white-dashed lines are the laminar flow interface (b) 2  $\mu\text{m}$  magnetic particles in device (c) 8  $\mu\text{m}$  magnetic particles in device (d) control image of particles following streamlines in the absence of a magnetic field. (e) 44  $\mu\text{m}$  magnetic particles undergoing positive magnetophoresis (f) calibration curve of fluorescent intensity of particle capture *via* concentration.



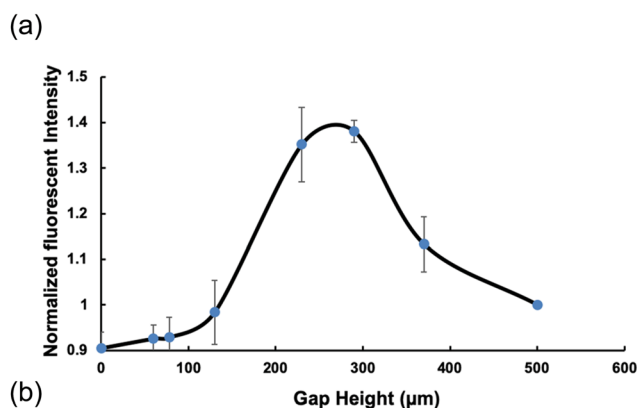
configuration, confirming that flow is extremely laminar. Based on the studies showing sustained high velocities, we were led to hypothesize that magnetophoresis was possible because fPADs have a large enough gap height for the majority of suspended particles to avoid being trapped in the cellulose fibers.<sup>4,19,23</sup>

We next sought to demonstrate laminar flow in the fPAD configuration because consistent laminar flow is needed for magnetophoresis to avoid convective mixing between the two parallel flowing streams in the H-cell.<sup>24</sup> A fPAD with two inlets containing red and green dyes showed a clear interface between the two liquid streams, again confirming laminar flow was established in the device with only slight diffusional mixing (Fig. 2a). Following the demonstration of fully developed laminar flow, the effect of inlet angle was quantified using the absolute mixing index (AMI) as a measure of total mixing. AMI indicates the extent of mixing and operates on a scale of 0–1, where 0 indicates a completely mixed state and 1 indicates a completely unmixed state. Photographs above each graph in Fig. 2b show each device and the main channel where the analysis is performed. Devices I, II, and III were all consistent with a 3 mm wide channel with only changing the angle of the inlet. Where device I had a 90° angle, device II had a 180° angle and device III had a 15° angle. Devices I and II showed inconsistent flow with relatively large standard deviation of  $\pm 1$  shown in blue. In device III a 15° angle between the two inlets led to less mixing and more reproducible laminar flow. Device IV was fabricated incorporating the optimal angle geometry with a 270°

fan at end of the channels that produces steady flow in paper analytical devices.<sup>21,25</sup> Inserting the fan decreased variability and increased AMI (Fig. 2b). Device IV showed the most reproducible laminar flow along with the least mixing denoted by an AMI of 0.7 with only diffusional mixing occurring. As a result, the device IV geometry was selected for subsequent studies.

### 3.2 Understanding particle behavior

Once velocities and laminar flow parameters were characterized, particle separation *via* magnetophoresis was investigated. Since the bottom layer of the fPADs was made from transparency film, it was possible to image the magnetic particles inside the gap. Fig. 3a shows a qualitative schematic of expected particle trajectories, where magnetic particles move across the laminar flow interface and are trapped by a permanent magnet. The NdFeB permanent magnet was placed on the top side of the device on the edge of the channel. 2  $\mu\text{m}$ , 8  $\mu\text{m}$ , and 44.1  $\mu\text{m}$  magnetic particles were tested. The sizes were selected based on commercial availability. 2  $\mu\text{m}$  and 8  $\mu\text{m}$  particles were retained within the paper fibers resulting in no observable movement across the parallel flowing streams and significant fluorescent background in the channel (Fig. 3b and c). Whatman 1 chromatography paper has an average pore size of 11  $\mu\text{m}$ , which resulted in trapping particles size smaller than 11  $\mu\text{m}$  in the device. In addition to particle size, the magnetic susceptibility changes proportionally with the size of the particles. As a result,



$$u_{\text{res}} = u_{\text{flow}} + u_{\text{mag}}$$

$u_{\text{res}}$  = velocity of particle

$u_{\text{flow}}$  = fluid velocity

$u_{\text{mag}}$  = magnetic velocity

# of Particles	# Particles Captured	# of Particles Left in Inlet	Actual Capture Efficiency	Theoretical Capture Efficiency
42 $\pm$ 5 (0.05 mg/mL)	25 $\pm$ 1	9 $\pm$ 2	62.5% $\pm$ 7.3	85.0%
90 $\pm$ 9 (0.1 mg/mL)	55 $\pm$ 3	22 $\pm$ 3	61.8% $\pm$ 6.3	85.5%
171 $\pm$ 18 (0.2 mg/mL)	108 $\pm$ 5	33 $\pm$ 4	63.5% $\pm$ 6.9	82.9%
399 $\pm$ 19 (0.3 mg/mL)	231 $\pm$ 14	124 $\pm$ 7	58.2% $\pm$ 3.0	89.1%

Fig. 4 (a) Optimization of particle capture with respect to gap height characterized by fluorescent intensity with correlated equation showing the relationship of the velocity of the particle with respect to the fluid and magnetic velocity. (b) Actual and theoretical capture efficiency in the device with an optimized gap height.

the 44.1  $\mu\text{m}$  particles remained in the gap area between paper and transparency film and could be moved across the laminar flow barrier with ease (Fig. 3d). The 44.1  $\mu\text{m}$  magnetic particles also accumulated near the magnet. As a control, the trajectories of the 44.1  $\mu\text{m}$  particles were obtained in the absence of a magnetic field. Without the field present the particles largely followed the liquid streamlines and did not cross the parallel streams' interface (Fig. 3e). The flow velocities of the particles follow velocities shown in Fig. 1c. The ability to pull the 44.1  $\mu\text{m}$  particles from one stream to another with the magnetic field under continuous flow is the first time magnetophoresis has been demonstrated in a pump-free device to the best of our knowledge.

After confirming magnetophoresis in ffPADs, the concentration dependent signal was evaluated by analyzing the fluorescence intensity of captured particles by taking the mean grey scale intensity of the area at magnet. Fig. 3f shows the normalized fluorescence intensity variation as a function of particle concentration. The linear calibration curve shows the

fluorescent signal increasing with increasing particle concentration with corresponding error bars taken from a standard deviation with an  $n$  of 3 for each concentration.

### 3.3 Improvements in device design

The effect of gap height on particle capture was investigated. Pamme *et al.* showed in a glass microchip that if fluid velocities are above 0.2  $\text{cm s}^{-1}$  then little to no deflection of magnetic particles occurs. Conversely, if velocities are lower than 0.04  $\text{cm s}^{-1}$  the magnetic moment will be more pronounced and inherently influence the particle deflection trajectory.<sup>26</sup> Since the velocity and magnetic field vectors are orthogonal, faster flow decreases particle deflection caused by a constant magnetic field, as described by the equation shown in Fig. 4. The fluid velocity in a ffPAD is controlled by the gap height between the layers, so the gap height was varied to study these competing effects.<sup>19</sup> ffPAD gap heights of 60, 70, 120, 230, 290, 360, and 500  $\mu\text{m}$  were tested using 44.1  $\mu\text{m}$  magnetic particles

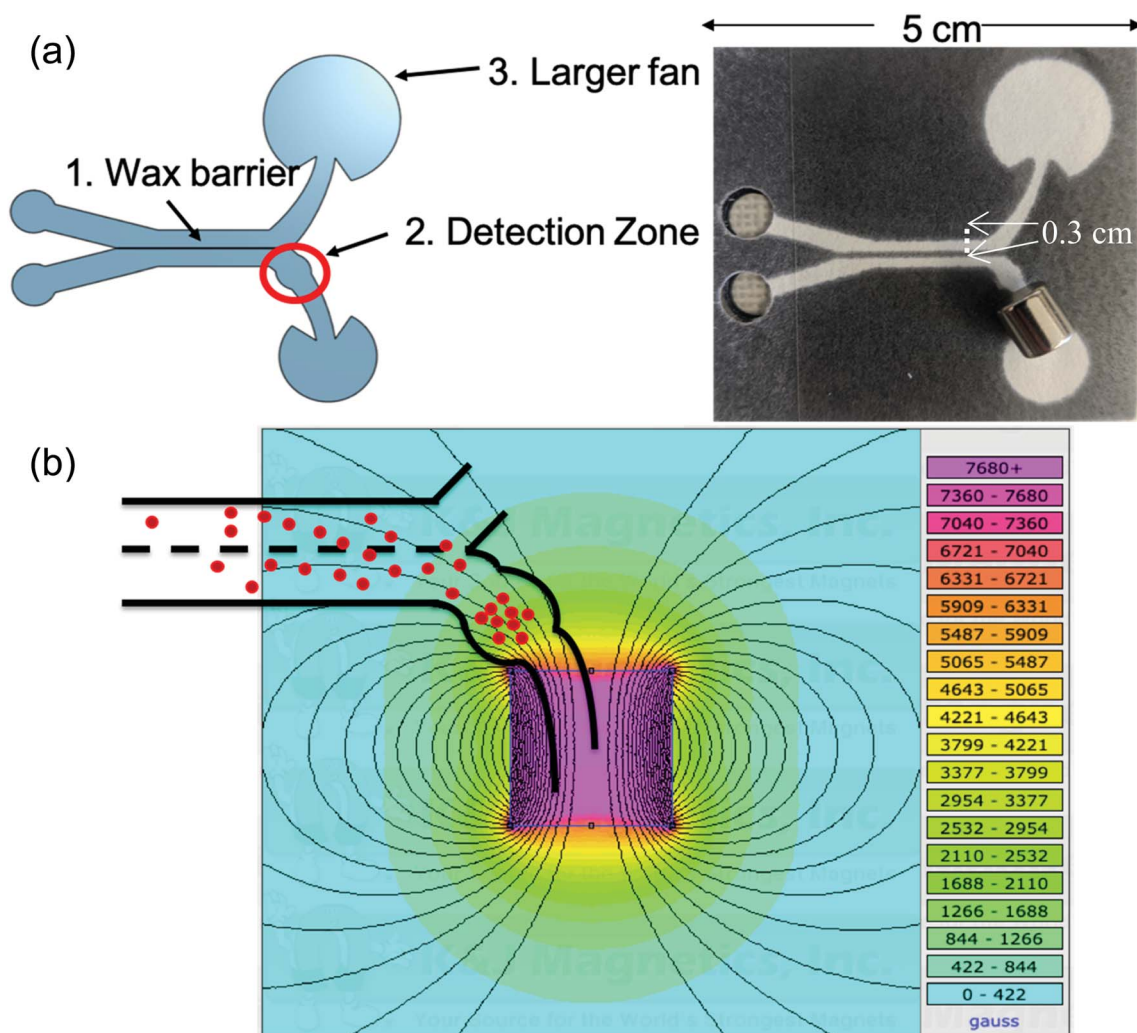


Fig. 5 (a) CAD rendering of device design and an actual image of the fabricated  $\mu\text{PAD}$ . (b) Magnetic field gradient of a N52 cylindrical NdFeB magnet overlay with channel, red spheres indicate magnetic particles. Magnetic flux density estimated to be 1300 gauss or 130 mT near the center of the channel (magnet image enlarged for viewing purpose).

and the fluorescent intensity of captured particles analyzed. A gap height between 230 and 290  $\mu\text{m}$  yielded the highest number of magnetic particles captured by the magnet (Fig. 4a). In the  $\mu\text{PAD}$ , a velocity exceeding  $\sim 1.5\text{ cm s}^{-1}$  prevented the particles from being captured. When the velocity was lower than  $\sim 0.5\text{ cm s}^{-1}$  the particles were retained in the paper fibers particle accumulation at the magnet was not observed.

In addition to optimizing gap height, the shapes of the outlet channels were studied. The magnetic particles follow a curved deflection trajectory. To account for this trajectory and improve the efficiency of particle capture, the device design was modified to match the general shape of the trajectory. A thin wax line was also printed on the top paper layer directly down the center of the channel to improve flow reproducibility. The particles then deflect only in the gap of the device and mixing in the paper is minimized. Additionally, a larger fan with a 14 mm diameter was used with the upper channel *versus* a 9.5 mm diameter fan on the lower channel. The larger fan is used to continually wick the solution from the upper channel and particle inlet to transport more particles to the detection zone and improve capture efficiency (Fig. 5). The magnetic field is shown with an overlay of a schematic of the device and magnetic particles following the field lines and being attracted toward the high gradient. The shape of the outlet channels were designed to match that of the magnet field lines to further improve capture of the magnetic particles.<sup>27</sup> After

optimization of the device was completed the capture efficiency was then investigated yielding capture of  $61.5\% \pm 5.8$  ( $n = 4$ ) with similar efficiencies for increasing concentrations. Other studies have shown capture efficiencies anywhere from 44% to 100% with permanent magnets, however all previous studies were conducted in traditional microfluidic channels using pumps.<sup>28</sup> Concentrations from  $0.05\text{ mg mL}^{-1}$  to  $0.3\text{ mg mL}^{-1}$  were selected because of the ability to physically count the number of particles in a  $30\ \mu\text{L}$  sample. The lowest capture was reported for the highest concentration because particles will aggregate at higher concentrations. The calculated capture efficiency of 61.5% was further analyzed and it was determined that many of the large  $44.1\ \mu\text{m}$  particles sediment to the bottom of the inlet and are trapped before reaching the capture magnet. If the particles left in the inlet were able to reach the capture zone, a theoretical yield of 85.6% would result (Fig. 4c). This is calculated by counting the number of particles left in the inlet *versus* the total number of particles added ( $n = 4$ ). A washing step of buffer immediately after the initial addition showed an increase of  $\sim 5\%$ .

### 3.4 *E. coli* magnetophoresis in urine

*Escherichia coli* (*E. coli*) is a common bacterium found in food and water that causes millions of infections per year in the US. *E. coli* accounts for 70–95% of all urinary tract infections

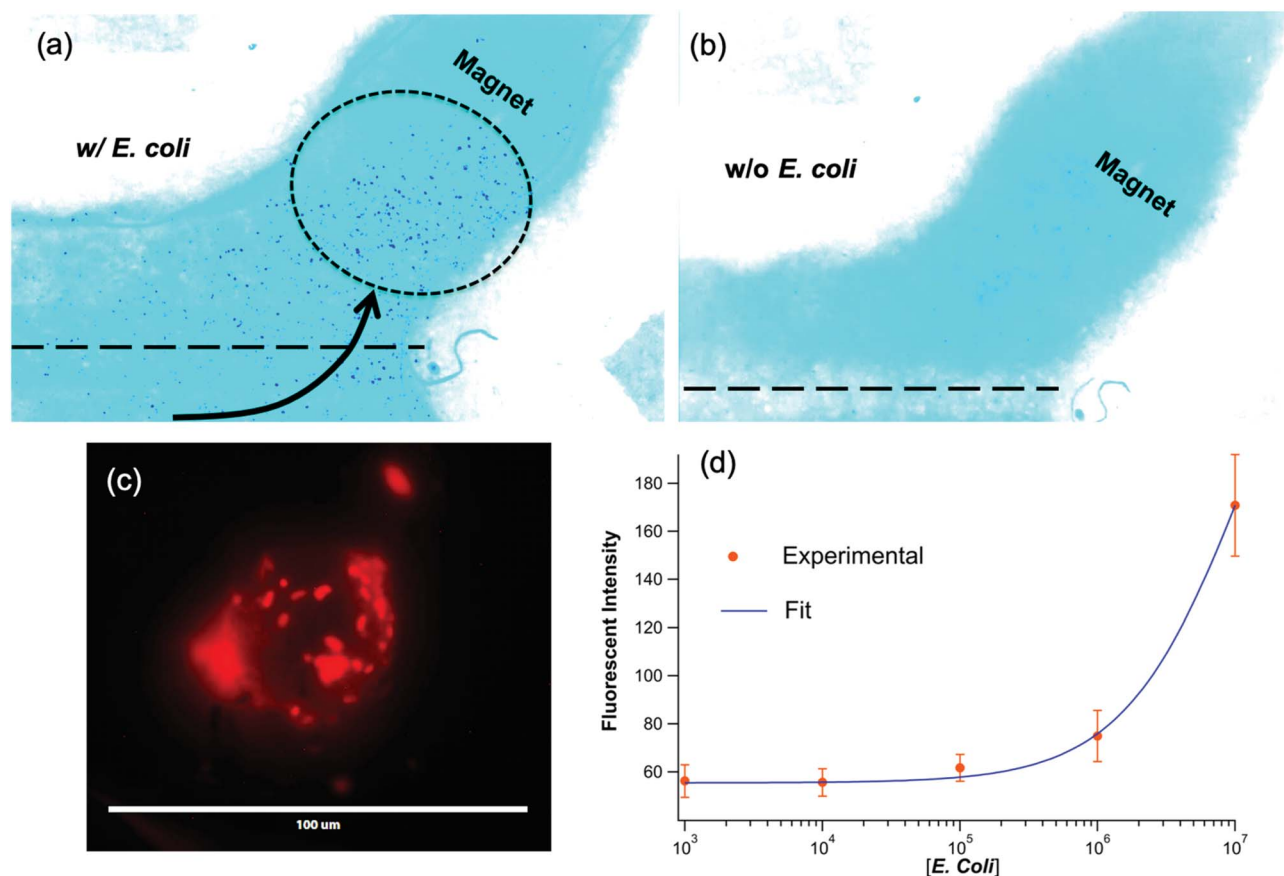


Fig. 6 Detection of fluorescently labeled bacteria in  $\mu\text{PAD}$  magnetophoresis. (a) Inverted image of positive magnetophoresis of *E. coli* complex. (b) Negative control assay (without *E. coli*). False color has been applied for visualization. (c) Fluorescent microscope image taken of bound *E. coli* to bead. (d) Dose-response curve of *E. coli* in urine in the device.

(UTIs).<sup>29</sup> An immunomagnetic sandwich *E. coli* assay in urine was performed to demonstrate the ability to carry out analysis on real samples. To verify that the 44.1  $\mu\text{m}$  beads would capture *E. coli*, the streptavidin coated beads were modified with biotinylated anti-*E. coli* and incubated with  $10^7$  CFU mL<sup>-1</sup> *E. coli* labeled with a fluorescent secondary antibody. As shown in Fig. 6c, fluorescently labeled bacteria are bound to the surface of the magnetic beads at  $10^7$  CFU mL<sup>-1</sup>. To demonstrate that the device could process a complex sample matrix, the optimized magnetophoresis assay was performed using human urine. 30  $\mu\text{L}$  of the streptavidin magnetic bead antibody complex was incubated in a urine sample spiked with *E. coli* during the antibody conjugation. A full schematic of the conjugation process can be found in the ESI.† After conjugation was complete, the complex was resuspended in urine and the detection of the labeled *E. coli* was shown in the device *via* magnetophoresis along with a blank (Fig. 6a and b) at  $10^7$  CFU mL<sup>-1</sup> of *E. coli* for the positive test. Next, serial dilutions from  $10^7$  CFU mL<sup>-1</sup> to  $10^1$  CFU mL<sup>-1</sup> were used to create a dose-response curve (Fig. 6d). The LOD in the device of  $10^5$  CFU mL<sup>-1</sup> is not as low as a colorimetric response seen previously by our group of  $10^2$  CFU mL<sup>-1</sup> for IMS methods,<sup>22</sup> but still demonstrates proof-of-concept. Detection limits could be improved in a few ways. First, enzymatic amplification instead of a fluorescent tag has been shown to improve the LOD especially in  $\mu\text{PADs}$ . Second, if the lower concentrations of *E. coli* were cultured prior to conjugation it would improve the LOD as well.<sup>30,31</sup> The final complex was introduced into the device and compared against the blank to see significant capture *E. coli* in the device in less than 30 s. Further investigation will be done to try to improve the capture efficiency with sequential washing steps to fully wash any complexes left in the inlet, and by adding a surfactant to the buffer to decrease particle-transparency interactions. Fluorescence detection is convenient for rapid detection of the complex, however we found it was limited by intensity when trying to record the entire channel.

## 4. Conclusions and future directions

In this work, the first example of a pump-free paper-based magnetophoresis device is demonstrated. The novel design shows efficient capture and detection of magnetic particles made possible by the fast flow system with sustained high velocities. Device dimensions, particle size, gap height, and magnet placement and strength were all studied to improve particle capture and reduce convective and diffusional mixing between the two flow streams. A capture efficiency of 61.5% was obtained and further investigation is being done to improve this as described above. Even though this capture efficiency is not as high as other magnetophoretic devices, this device represents a novel approach to a technique that has not previously been demonstrated in paper. The current method for this assay involves several off-chip steps, but future work will also seek to integrate all steps to minimize assay complexity. We envision additional new potential diagnostic platforms possible because of the technique described. Future work will target adapting the

system to incorporate the off-chip manipulations onto the device and to detect multiple pathogens at once.

## Conflicts of interest

There are no conflicts to declare.

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